

Advanced Propulsion Workshop -2017

Entanglement Drive Analysis of the Mach Effect Thruster

Glen A. Robertson

Part 2

Generalized Form of a

New Non-Gravitational Acceleration Equation

**Acceleration of the Density Field
(Like a Warp Bubble)**

Object's Acceleration

$a_c \equiv a_{\phi_c} = 6 \left(\phi^3 \sqrt{\frac{R_{\phi_a}}{l_p}} \right)^{1/2}$

Estimated Radius of the Accelerated Density Field

Phase Factor

Unit Vector

$\hat{\phi}$

Local Acceleration of Gravitation

Planck Length

$c \equiv$ object under study

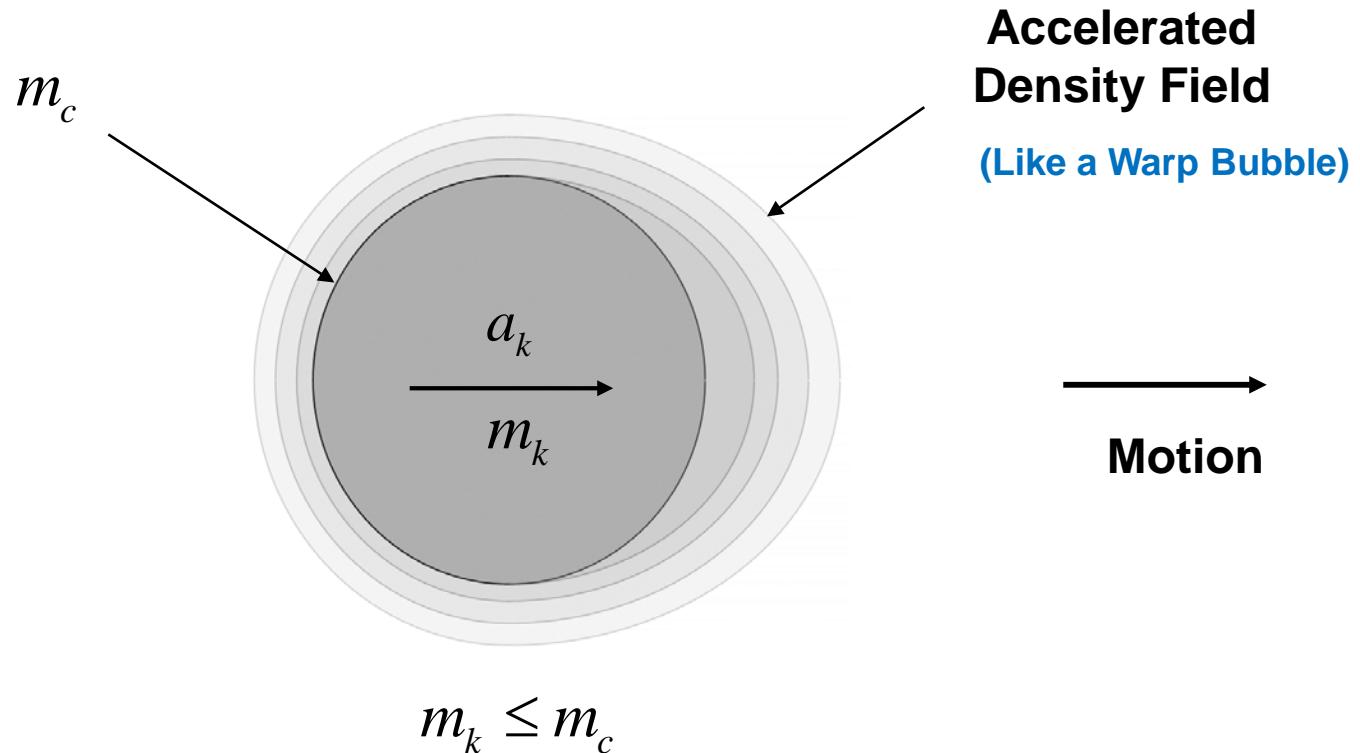
$\phi \equiv$ Density Field

$\phi_a \equiv$ Accelerated Density Field

$M \equiv$ Local Gravitation Source

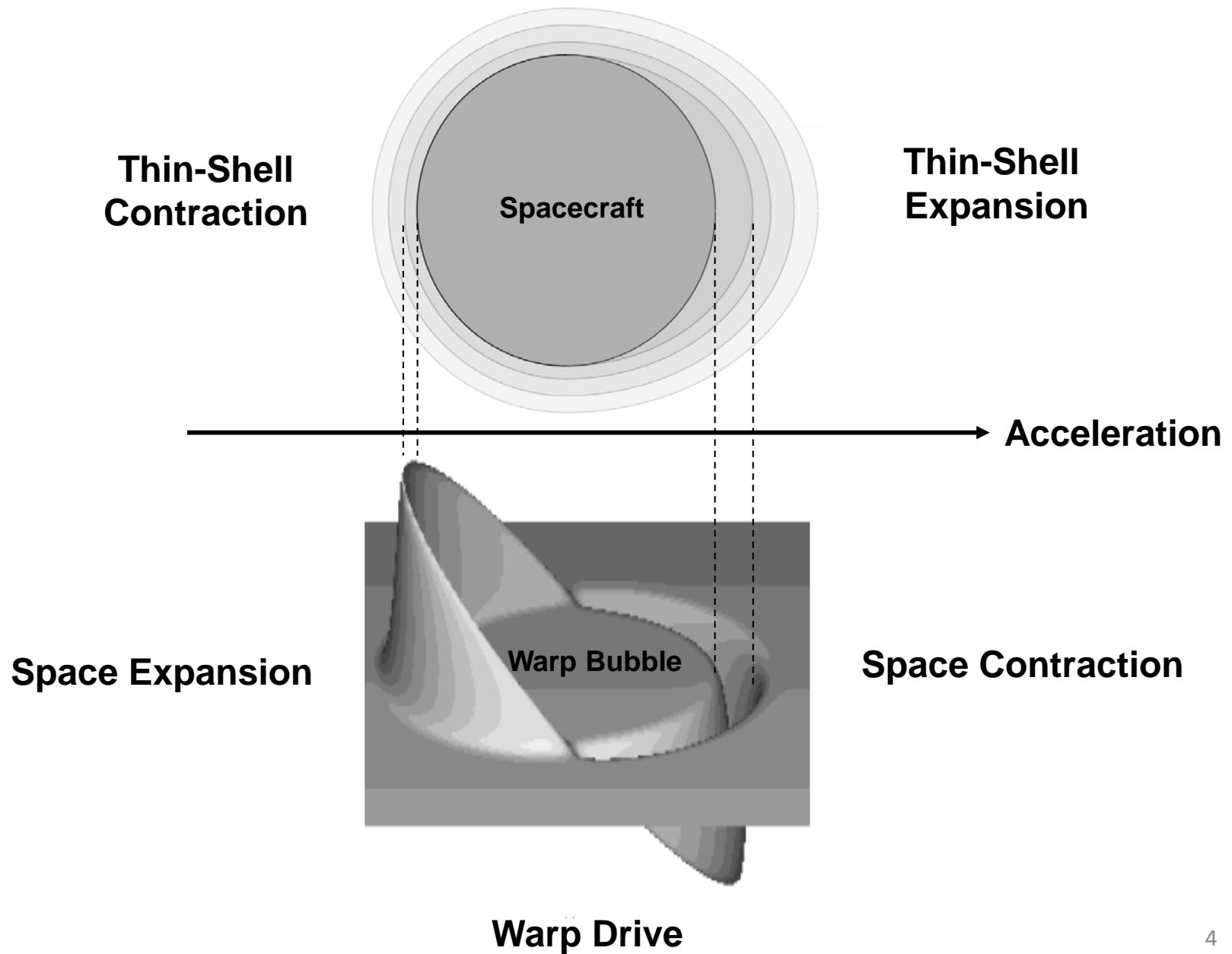
Like a time change ratio between the Warp Bubble and the reaction mass in the Warp Bubble with respect to its effect on the Universe

ACCELERATION MECHANISM



$c \equiv$ object under study

$k \equiv$ accelerated mass in the object under study



Phase Factor

$$\varphi \equiv \frac{\text{time rate of change of the Warp Bubble}}{\text{time rate of change of the accelerated } m_k} \quad \alpha_U \approx \left(\frac{dt_\phi}{dt_k} \right) \alpha_U$$

$$\alpha_U \equiv \frac{\text{Universe normalization of } dt_k}{\text{Universe normalization of } dt_\phi} = \frac{dt_{k_U}}{dt_{\phi_U}}$$

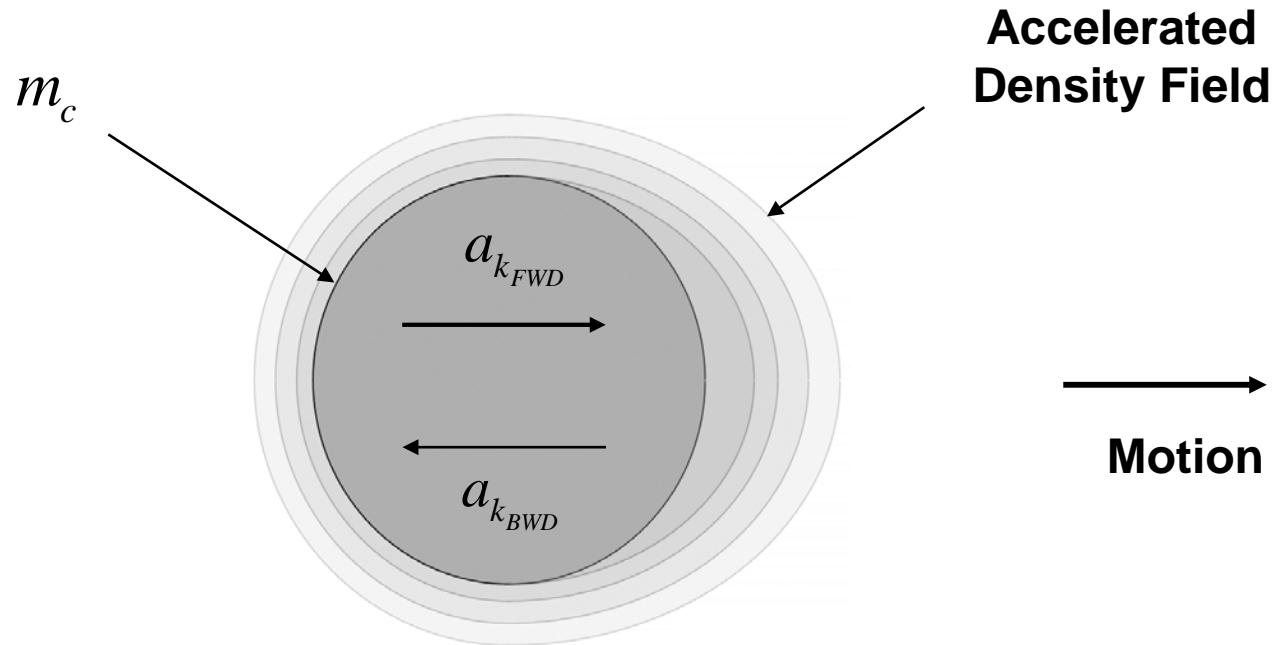
$dt_\phi \approx dt_{\phi_U}$ **Implies a Mach Effect System**

Estimated Radius of the Accelerated Density Field

$$R_\phi = \frac{R_c}{\left(1 + \left(\frac{a_k}{g_M} \right) \left(\frac{m_k}{m_c} \right) \right)^{1/3}}$$

ACCELERATION MECHANISM

Entanglement Drive



$$a_{k_{FWD}} > a_{k_{BWD}}$$

$$m_k \leq m_c$$

ACCELERATION MECHANICS FOR ENTANGLEMENT DRIVE

$$a_{\phi_c} \equiv a_{\phi_{ED}} \approx f_{A_{FWD}} dt_{\phi_{FWD}} a_{\phi_{FWD}} - f_{A_{BWD}} dt_{\phi_{BWD}} a_{\phi_{BWD}}$$

$f_A \equiv$ Frequency of the accelerated mass

$dt_\phi \equiv$ Time rate of change of the density field

ACCELERATION MECHANICS FOR ENTANGLEMENT DRIVE

$$\varphi_{FWD} \approx \left(\frac{1}{\eta_{\phi_{FWD}} \eta_{k_{FWD}}} \right) \left(\frac{1}{M_E^2 (d_{k_{FWD}} R_c)} \right)$$

$$\varphi_{BWD} \approx \left(\frac{1}{\eta_{\phi_{BWD}} \eta_{k_{BWD}}} \right) \left(\frac{1}{M_E^2 (d_{k_{BWD}} R_c)} \right)$$

(Type I)

$$R_{\phi_{FWD}} = \frac{R_c}{\left(1 + \left(\frac{a_{k_{FWD}}}{g_M} \right) \left(\frac{m_{k_{FWD}}}{m_c} \right) \right)^{1/3}}$$

$$R_{\phi_{BWD}} = \frac{R_c}{\left(1 + \left(\frac{a_{k_{BWD}}}{g_M} \right) \left(\frac{m_{k_{BWD}}}{m_c} \right) \right)^{1/3}}$$

(Type II)

m_k and a_k are unknown

d_k is estimated from test object

R_ϕ is estimated from test data

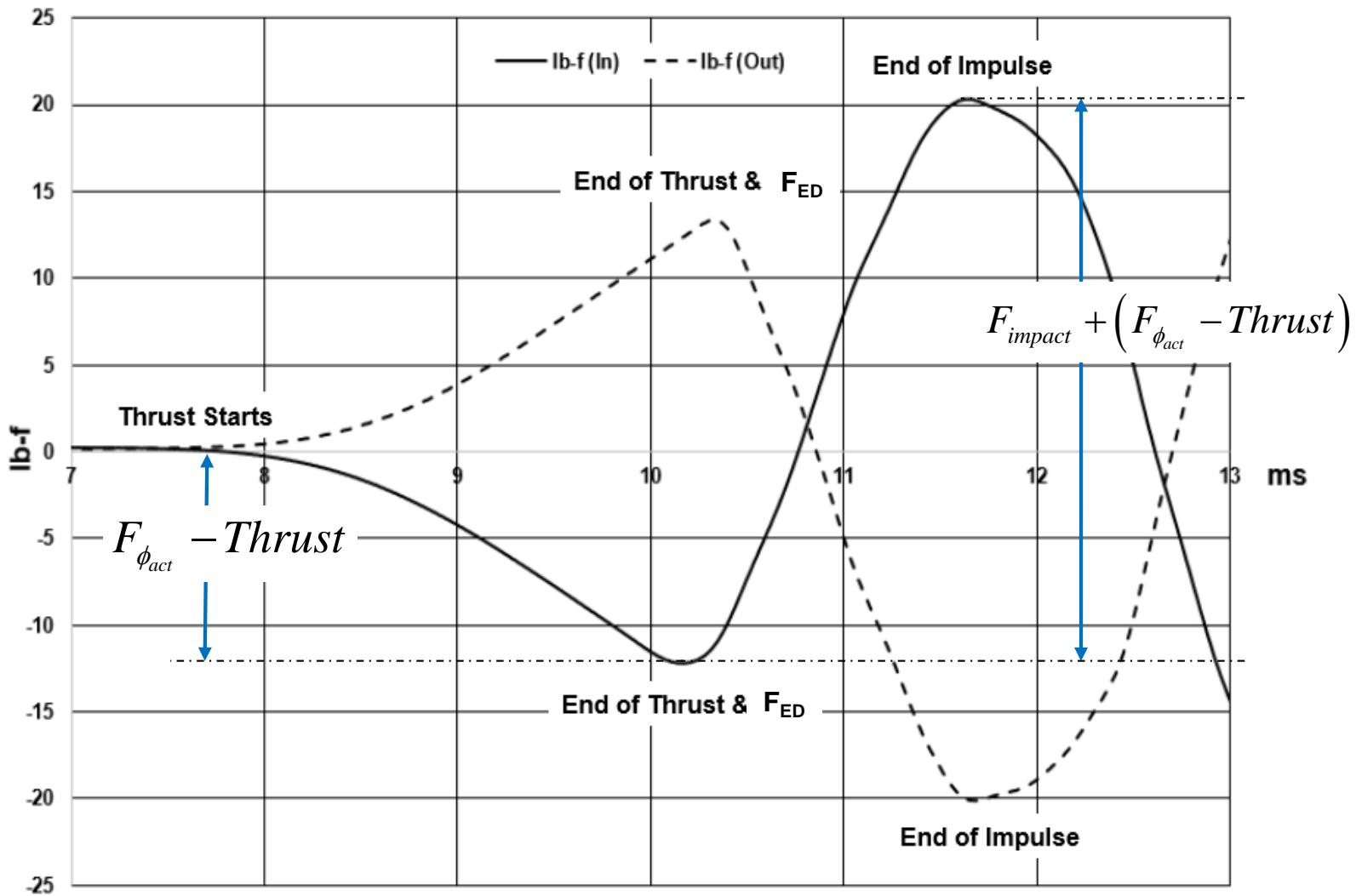
Cosmological Energy Scale Factor.

$$M_E \approx \left(\frac{\Lambda}{8\pi l_p^2} \right)^{1/4} \approx 11378 \text{ } m^{-1}$$

Λ - Cosmological Constant

Dual Position Latching Actuator Test

Single Impulse



Entanglement Drive

Dual Position Latching Actuator

$$F_{\phi_{act}} \approx m_{act} a_{\phi_{act}} \approx 91.38 \text{ N } (\square 20.54 \text{ lbs})$$

$$a_{\phi_{act}} \approx 6 \left(\varphi_{act}^3 \sqrt{\frac{R_{\phi_{act}}}{l_p}} \right)^{1/2} \quad g_N \approx 404.34 \text{ m/s}^2$$

Single Impulse

$$R_{\phi_{act}} \approx \left(1 + \left(\frac{a_{arm}}{g_{\oplus}} \right) \left(\frac{m_{arm}}{m_{act}} \right) \right)^{-1/3} \quad R_{act} \approx 0.0085 \text{ m}$$

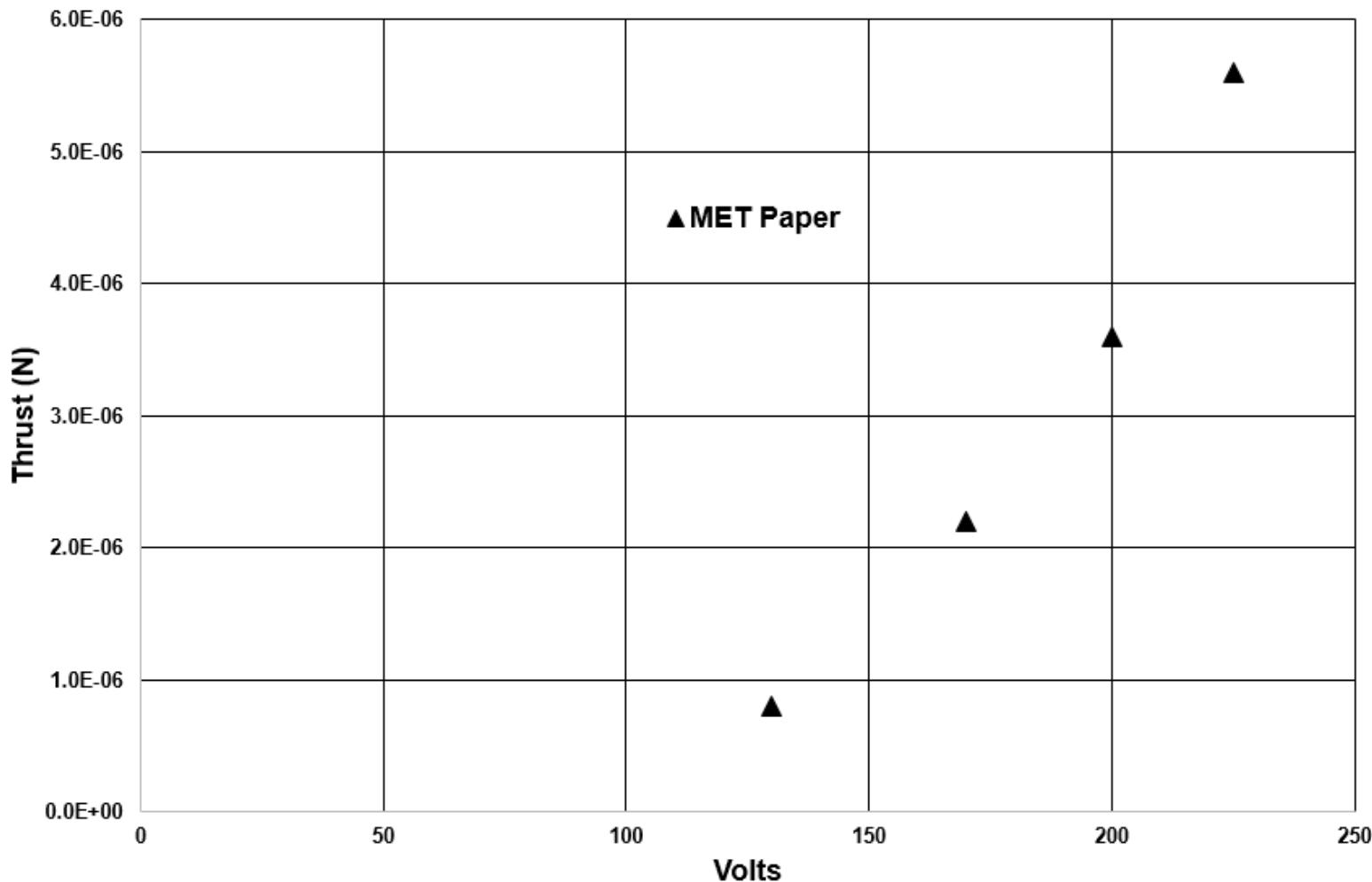
$$\varphi_{act} \approx \eta \left(\frac{1}{8\pi M_E^2 d_{arm} R_{act}} \right) \approx \eta (1.24 \times 10^{-5})$$

Type I

$$\eta_{\phi} \eta_k = 8\pi/\eta \quad \eta = 1.0256$$

PZT - Mach Effect Thruster

Frequency Modulated



Entanglement Drive

PZT - Mach Effect Thruster

Frequency Modulated

Voltage

$$F_{\phi_V} = m_{MET} \left(f_A dt_{\phi_V} \mathbf{a}_{\phi_V} \right) \approx \frac{9}{2} f_A \left(\frac{R_{\phi_V}}{c} \right) \left(\varphi_V^3 \sqrt{\frac{R_{\phi_V}}{l_p}} \right)^{1/2} W_c \hat{\phi}$$

$$dt_{\phi_V} = \frac{3}{4} \left(\frac{R_{\phi_V}}{c} \right) \quad W_c = m_{MET} g_{\oplus}$$

$$\mathbf{a}_{\phi_V} \approx 6 \left(\varphi_V^3 \sqrt{\frac{R_{\phi_V}}{l_p}} \right)^{1/2} g_M \hat{\phi}$$

Entanglement Drive

PZT - Mach Effect Thruster

Frequency Modulated

$$M_E \approx \left(\frac{\Lambda}{8\pi l_p^2} \right)^{1/4}$$

$$\varphi_V \approx \frac{3}{4\pi} \left(\frac{1}{M_E R_c} \right)$$

$$dt_\phi \approx dt_{\phi_U} \longrightarrow R_{\phi_V} \approx (M_E d_{k_V}) R_c$$

A Mach Effect System

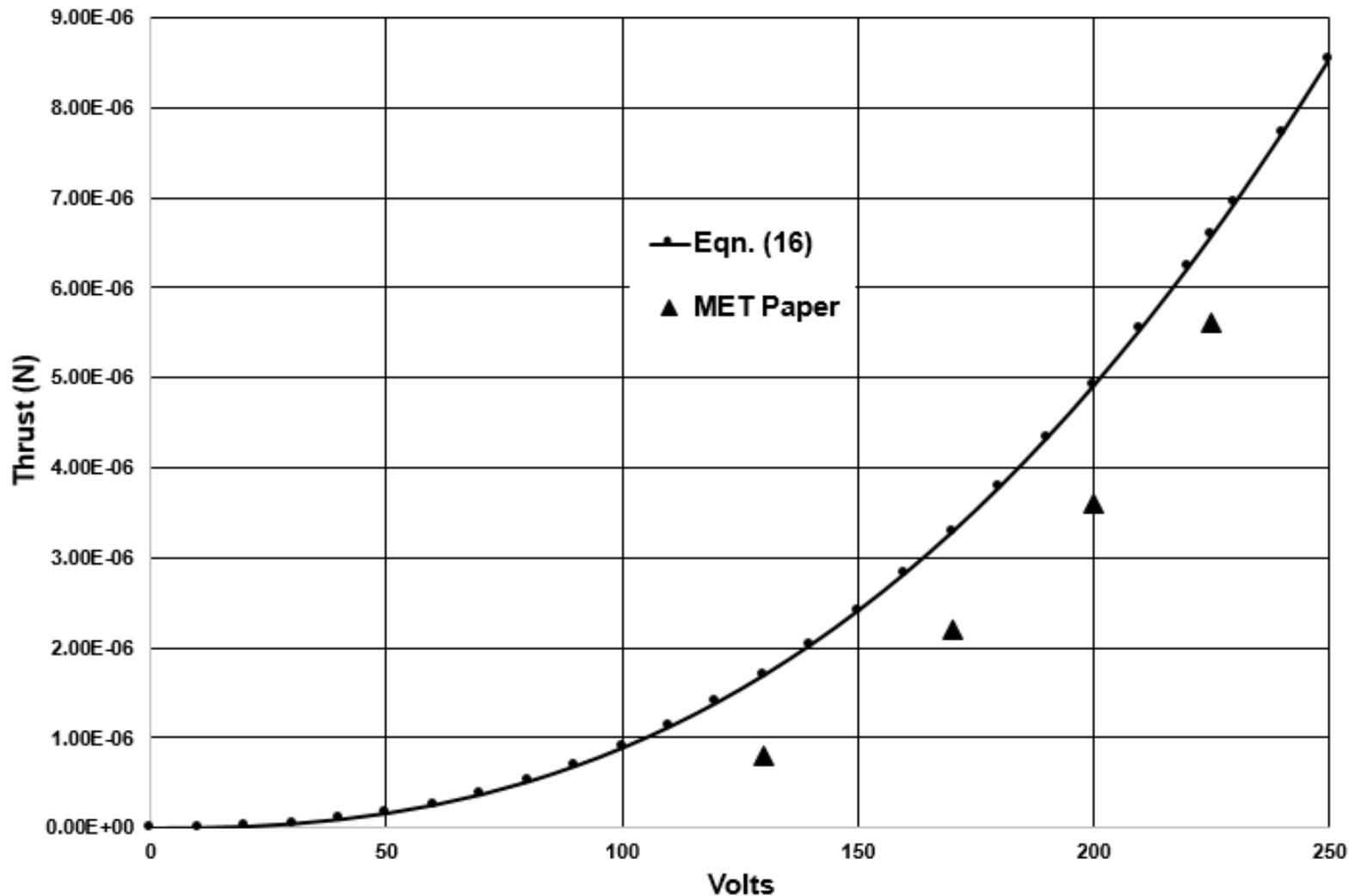
$$d_{k_V} = (K_p V + K_e V^2) x_0$$

Type II

$$\varphi_V \approx \left(\frac{1}{\eta_{\phi_V} \eta_{k_V}} \right) \left(\frac{1}{M_E^2 (d_{k_V} R_c)} \right) \approx \frac{dt_\phi}{dt_k} \frac{dt_{k_U}}{dt_{\phi_U}}$$

PZT - Mach Effect Thruster

Frequency Modulated



Entanglement Drive

PZT - Mach Effect Thruster

Frequency Modulated

$$F_{\phi_M} \approx f_A dt_{\phi_M} a_{\phi_M} \approx \frac{9}{2} f_A \left(dt_{\phi_M} \left(\varphi_M^3 \sqrt{\frac{R_{\phi_M}}{l_p}} \right)^{1/2} \right) W_c \approx 10^{-6} N$$

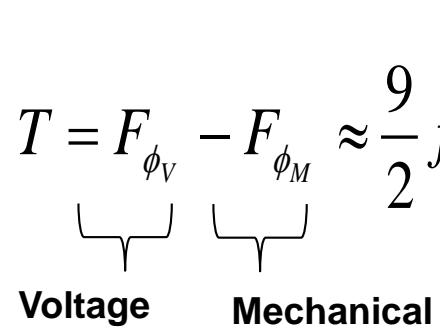
Mechanical

Entanglement Drive

PZT - Mach Effect Thruster

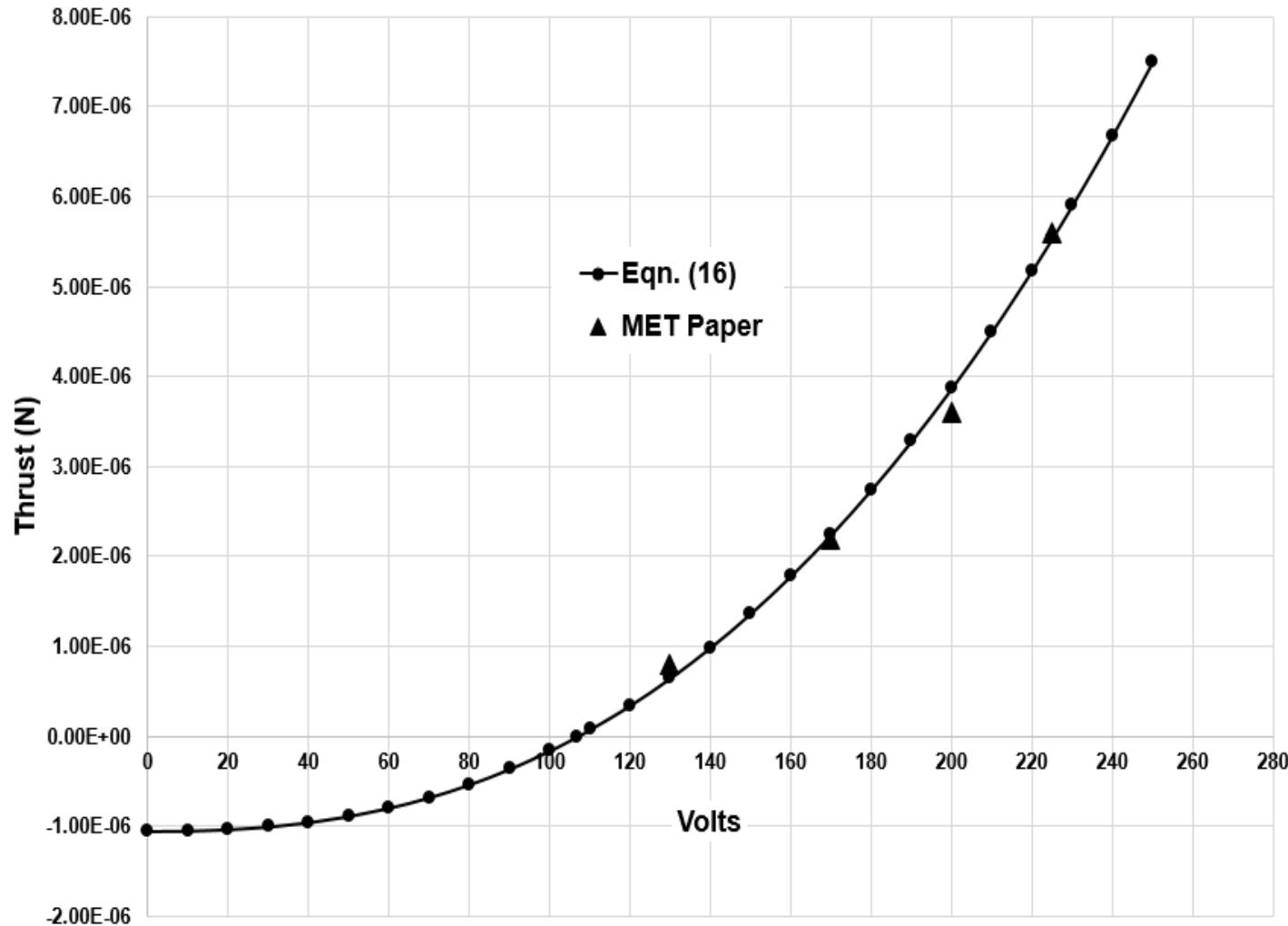
Frequency Modulated

$$T = F_{\phi_V} - F_{\phi_M} \approx \frac{9}{2} f_A \left(\left(\frac{R_{\phi_V}}{c} \right) \left(\varphi_V^3 \sqrt{\frac{R_{\phi_V}}{l_p}} \right)^{1/2} \right) W_c - 10^{-6} N$$


Voltage Mechanical

PZT - Mach Effect Thruster

Frequency Modulated



THE ACCELERATION EQUATION FOR:

MACH EFFECT THRUSTERS
OR
NEW PROPELLANT-LESS SPACE DRIVES
OR
WARP DRIVES

$$a \approx f_{A_{FWD}} dt_{\phi_{FWD}} a_{\phi_{FWD}} - f_{A_{BWD}} dt_{\phi_{BWD}} a_{\phi_{BWD}}$$

Where all you need to know is the internal reaction mass and its

- Forward and backward accelerations, and
- Frequency of the internal mass acceleration.

Forward Work

$$a_{\phi_c} = 6 \left(\varphi^3 \sqrt{\frac{R_{\phi_a}}{l_p}} \right)^{1/2} g_M \hat{\phi}$$

$$\ln \left(\frac{a_k}{g_M} \right) \sqrt{1 - (a_k dt)^2 / c^2} \approx 6 \quad \text{For current test data}$$

Lorentz Factor

- To drive the field acceleration to zero at the acceleration of gravity, and
- Prevent a violation of the conservation of energy at the speed of light